

Acceleration Levels of Dropped Objects

Technical Paper 321 By Peter Leonhardt

Introduction

This paper is intended to provide an overview of drop shock testing, which is defined as the acceleration experienced by an object dropped onto a hard surface. The practical application of this work is to characterize the acceleration levels generated when an accelerometer is dropped onto a rigid surface. Similar dynamic responses can be inferred to the object on which the accelerometer is mounted.

An accelerometer is a particularly convenient object to evaluate, since it may directly characterize the amplitude and pulse width generated from an impact. Many accelerometers have maximum acceleration ratings which are sufficient to measure high acceleration levels in a wide variety of applications. It should be realized that in almost every case, ratings may be exceeded by seemingly benign handling shocks.

Summary

It has been demonstrated that when dropped from a height of one meter, objects may impact rigid surfaces with very large accelerations. Relatively speaking, lower mass objects tend to result in greater accelerations. As an example, an accelerometer, with a normal mass of only 10 grams, may easily be subjected to 30 000 g when dropped from one meter onto a rigid steel plate. If the interface on impact is flat-to-flat, the level may exceed 80 000 g.

The amount of acceleration imparted to a dropped object is proportional to the square root of the drop height, and the inverse of the pulse width.

The drop shock

Consider an object dropped onto a horizontal surface. For the purpose of this evaluation, the object starts at rest, and free-falls to impact a rigid surface after traveling a distance, d_1 , as shown in Figure 1. After impact, the object rebounds upward to some height d_2 .



Figure 1

An object in free-fall experiences constant acceleration due to gravity, and the velocity increases in the downward (negative) direction as

$$v(t) = g t$$
⁽¹⁾

The distance traveled is

$$d(t) = \frac{1}{2} g t^2$$
⁽²⁾

These two equations may be combined to determine the velocity of the object immediately prior to impact.

$$v_1 = -\sqrt{2 g d_1}$$
 (3)

Likewise, the upward velocity immediately after impact is

$$v_2 = \sqrt{2 g d_2}$$
 [4]

Immediately before impact, the object is still in free-fall. If the object were a piezoelectric accelerometer, it would have zero output. The same is true immediately after impact. During impact, the object must stop its downward course, and reverse its direction. This is where the high level acceleration occurs. Acceleration is, by definition, the rate of change of velocity. The faster the object changes from downward velocity to upward velocity, the greater the acceleration.

$$a = \frac{\Delta v}{\Delta t}$$
(5)

Paraphrasing Newton, an object in motion tends to remain in motion ... and a more massive object requires more force to accelerate it. This implies that, in general, more massive objects take more time to rebound. Consider two objects of equal shape and rigidity, one more massive than the other. Both fall and rebound the same distance, so the change of velocity is equal in both cases. However, the more massive object takes more time to rebound (and has a longer pulse width), so Δt is greater, resulting in less acceleration as shown by equation (5). For this reason, when dropped from the same height, lighter objects will tend to exhibit shorter pulse widths and greater acceleration levels. The force imparted to the floor is greater with a more massive object, but the acceleration is less. The mathematics to follow further substantiates this.

The half sine pulse

When describing the output of an accelerometer during a drop shock, the wave shape is often

referred to as a half sine. Few impact wave shapes are truly half sine, but the resemblance is usually close enough. The half sine is also a simple function to treat mathematically, and it will be used as a model to predict the behavior of drop shock phenomena. A plot of acceleration versus time of a half sine shock will look something like that shown in Figure 2.



The velocity is the integral of the acceleration, plus an integration constant. Integrating the half sine results in a 'half cosine', and would look something like that shown in Figure 3, below. Keep in mind that the curve can be shifted vertically to match the boundary conditions of the drop (thanks to the integration constant).





To set the boundary conditions of the velocity curve, first realize that v1 is simply the velocity immediately before impact.

$$v_1 = -\sqrt{2 g d_1}$$
 [6]

And v2 is the velocity immediately after impact

$$v_2 = \sqrt{2 g d_2}$$
⁽⁷⁾

The curve of figure 3 with the above two boundary conditions is described by

$$v(t) = \cos\left(\frac{\pi t}{T}\right) \left(\frac{v_1 - v_2}{2}\right) + \frac{v_1 + v_2}{2}$$
(8)

where T is the pulse width of the impact. Taking the derivative of the velocity function yields the acceleration function

$$a(t) = \frac{d}{dt} v(t) = \frac{d}{dt} \left(\cos\left(\frac{\pi t}{T}\right) \left(\frac{v_1 - v_2}{2}\right) + \frac{v_1 + v_2}{2} \right)$$
 [9]

$$a(t) = \frac{\pi}{T} \sin\left(\frac{\pi t}{T}\right) \left(\frac{v_1 - v_2}{2}\right)$$
 [10]

such that

a(0) = 0 (11)

$$a\left(\frac{T}{2}\right) = \frac{\pi}{T}\left(\frac{v_2 - v_1}{2}\right)$$
⁽¹²⁾

$$a(T) = 0$$
 [13]

all which describe the characteristics of a half sine acceleration pulse. The peak acceleration occurs at time T/2, as seen in equation (12). Substituting the velocity variables,

$$a_{\flat} = a\left(\frac{T}{2}\right) = \frac{\pi}{T}\left(\frac{v_2 - v_1}{2}\right)$$
⁽¹⁴⁾

$$a_{p} = \frac{\pi}{T} \left(\frac{\sqrt{2 g d_{2}} - \left(-\sqrt{2 g d_{1}} \right)}{2} \right)$$
(15)

$$a_{\mu} = \frac{\pi}{T} \sqrt{\frac{g}{2}} \left(\sqrt{d_2} + \sqrt{d_1} \right)$$
 [16]

From equation (16) it can be seen that the peak acceleration in a drop shock is primarily dependent on two things:

- 1. The inverse of the pulse width. Shorter pulse widths result in higher accelerations.
- 2. The square root of the drop and rebound distance. Assuming minimal rebound, doubling the drop height results in a 41% higher shock.

Here are some simplified approximations:

$$g_{peak} = .71 \frac{\sqrt{d_2} + \sqrt{d_1}}{T}$$
 for $d_{1'} d_2$ in meters: T in seconds [17]

$$g_{peak} = .39 \frac{\sqrt{d_2} + \sqrt{d_1}}{T}$$
 for d_1 , d_2 in feet: T in seconds [18]

The pulse width 'T' is dependent on the shape and material properties of the dropped object and the impact surface.

Simple prediction model of drop shocks

For generalization purposes, consider the dropped object a solid mass of some material. When the dropped object impacts a rigid surface, the object deforms (compresses), and may rebound back upwards. For simplicity, assume no rebound.

The dropped object has mass m, and modulus E. The distance the object compresses is x. From basic formulae

$$\mathbf{F} = \mathbf{k} \mathbf{x} \tag{20}$$

we can find the acceleration imparted at the maximum compression distance, x. This is what we want.

$$a = \frac{k x}{m}$$
(21)

During the shock,

$$v = \sqrt{2 a x}$$
 (22)

$$x = \frac{v^2}{2a}$$
(23)

Substituting (23) into (21) yields

$$x = \frac{k \frac{v^2}{2a}}{m}$$
(24)

$$a^{2} = \frac{k v^{2}}{2 m}$$
 (25)

The spring constant of a bulk spring can be expressed in terms of the modulus, the area being compressed and the height.

$$k = \frac{E A}{h}$$
 (26)

Substituting (22) and (26) into (25) yields

$$a^{2} = \frac{\frac{E A}{h} \left(2 g d_{1} \right)}{2 m}$$

$$[27]$$

which simplifies to

$$a = \sqrt{\frac{E \ A \ g \ d_1}{h \ m}}$$
(28)

Note:

- h = solid height of the equivalent bulk spring or thickness of item being dropped
- d1= height of the dropped object

E = modulus

- A = area being compressed
- m = mass of spring
- g = acceleration

From this basic equation, a number of conclusions can be deduced.

- Greater acceleration levels will be achieved when the surface area, A, is increased. Specifically, if an object is dropped onto its most flat surface (flat-on-flat impacts) the acceleration is the greatest. Conversely, if dropped onto a sharp corner, the acceleration will be minimized.
- 2) Greater acceleration levels will be achieved with a higher drop (this should be obvious).
- *3) Greater acceleration levels will be achieved with a lower mass object.*
- 4) Greater acceleration levels will be achieved with a stiffer object (higher modulus).

The following table shows the estimated peak acceleration levels at various drop height and pulse width.

inch –	\rightarrow	6	12	24	36	48	60
pulse width msec ↓	0.010 0.013 0.016 0.020 0.025 0.032 0.040 0.050 0.063 0.079 0.100 0.13 0.16 0.20 0.25 0.32 0.40 0.50 0.63 0.79 1.0 1.3 1.6 2.0 2.5 3.2 4.0 5.0 6.0 8.0 10 12 16 25 3.2 4.0 5.0 6.0 8.0 10 12 16 25 3.2 4.0 5.0 6.0 8.0 10 12 16 25 3.2 4.0 5.0 6.0 8.0 10 1.0 1.0 1.0 1.0 1.0 1.0 1.	28000 21000 17000 14000 5500 4400 3500 2800 2200 1700 1400 1100 870 690 550 440 350 280 220 170 140 350 280 220 170 140 110 87 69 55 46 34 28 23 17 14 11 9 7 6 4 4 3	39000 30000 24000 16000 12000 7800 6200 4900 3900 3100 2500 2000 1600 1200 1600 1200 390 310 250 200 160 120 1000 780 620 490 390 310 250 200 160 120 390 310 250 200 160 120 1000 780 620 490 310 250 200 160 1200 1600 1200 1000 780 620 100 250 200 1600 1200 1000 780 620 100 250 200 160 120 100 250 200 160 120 100 250 200 160 120 100 120 100 250 200 160 120 100 120 100 250 200 160 120 100 10	55000 42000 34000 28000 22000 17000 14000 5500 4400 3500 2200 1700 1400 1100 870 690 550 440 350 280 220 170 1400 350 280 220 170 140 350 280 220 170 140 350 280 220 170 140 350 280 220 170 1400 1100 870 690 550 440 350 280 220 170 1400 1100 870 690 550 440 350 280 220 1700 1400 2800 2200 1700 2800 2200 1700 2800 2200 1700 2800 2200 1700 550 440 350 280 220 1700 1400 1100 870 690 550 440 350 280 220 170 1400 1100 870 690 550 440 350 280 220 170 1400 1100 870 690 550 440 350 280 220 170 1400 1100 870 690 550 440 350 280 220 170 1400 1400 1400 1400 1400 1700 1400 14	68000 52000 42000 34000 27000 17000 14000 17000 3400 2700 2100 1700 1300 1700 1300 1100 850 680 540 430 340 270 210 1700 130 110 850 680 540 430 340 270 210 1700 130 110 850 680 540 430 340 270 210 1700 2100 1700 21000 17000 21000 17000 21000 17000 21000 21000 17000 21000 17000 2100 2100 2100 2100 2100 2100 2100 2100 2100 2100 2100 2100 2100 2100 2100 2100 210 21	78000 60000 49000 39000 24000 20000 16000 12000 12000 3900 3100 2500 2000 1600 1200 160 1000 780 655 49 39 31 250 200 160 100 78 65 49 39 31 250 200 160 130 100 78 65 49 39 31 25 20 160 130 100 78 65 49 39 31 25 20 160 130 100 78 65 49 39 31 25 20 16 120 100 78 65 49 39 31 25 20 16 1200 160 1200 180 100 78 65 49 39 31 25 20 16 12 10 8 8	87000 67000 55000 44000 35000 27000 22000 17000 14000 5500 4400 3500 2200 1700 1400 1100 870 690 550 440 350 2200 1700 1400 350 280 220 170 150 110 87 55 44 355 280 220 170 150 110 87 73 55 44 35 28 22 17 14 35 28 22 17

Measuring a dropped object

Due to the high level of acceleration generated during the drop impact, selecting the right accelerometer and signal conditioner is critical to a good measurement. A few areas need special attention:

1. Size of the object to be Measured-If the selected accelerometer is too big, its presence may alter the response characteristics of the object. As a rule of thumb, the accelerometer should not be more than 10th of the weight of the measured object.

2. Accelerometer mounting-Although the mounting method is practically dictated by the selected accelerometer, it is important to keep in mind that screw mounting is preferred in shock environments.

3. Type of measurement-Are you trying to measure the rigid body motions of the dropped object (i.e., how much does it bounce), or are you interested in the peak acceleration responses of the object? If rigid body motions are desired, the measurement instrumentation chain must have DC response in order to minimize zero-offset errors.

4. Dynamic characteristics of accelerometer-

The accelerometer must have the proper frequency response and dynamic range. It is recommended to use the table above as a guide and apply a safety margin of 2 in reaching the desired specifications. For more information on selecting the right accelerometer, refer to TP291 Accelerometer Selection Based on Application, available for download at www.endevco.com.

5. Transfer characteristics of amplifier-Given the high level and wide bandwidth signal output from the accelerometer, the amplifier must handle the signals without producing spurious distortion. Frequency and overload characteristics of the amplifier must be well understood before making a selection.

6. Frequency range and Resolution of analog-

to-digital conversion-Attention must be paid in selecting the proper bit and sampling rates in A/D converter. Sampling rate must be high enough to cover the bandwidth of the acceleration signals, which can sometime exceed 200 kHz. Sufficient bit resolution is critical for deriving rigid body motion information from an accelerometer. Depending on the desired accuracy, low bit rate can result in gross integration errors during signal post processing.



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